



cigre
Nederland

1 February 2024

Towards net-zero emission of T&D grids



The current status of SF₆-free high-voltage equipment

René Smeets – KEMA Labs



cigre

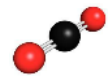
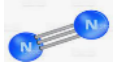
For power system expertise

KEMA Labs

SF₆ gas alternatives

- Insulation: GIS, GIL, GIB, instrument transformers
- Switching (current interruption): Circuit breakers, switches, disconnectors

natural-origin gases

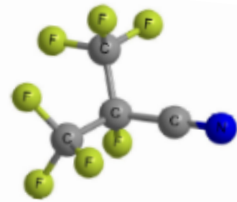


} air

various mixtures

- GWP < 1
- Insulation only
(switching in vacuum)

fluoronitriles



Novec™ 4710

C4-FN

g³

5 % in a mixture with CO₂ (and mostly O₂)

- GWP 2750
- In mixture GWP < 1000
- F-gas, PFAS substance
- Insulation and switching

fluoroketones



Novec™ 5110

C5-FK

Airplus

Abandoned by industry:
HV equipment 2021
MV equipment 2023

Abandoned by industry:
HV equipment 2021
MV equipment 2023

- GWP < 1
- In mixture GWP < 1
- PFAS substance
- Insulation and switching

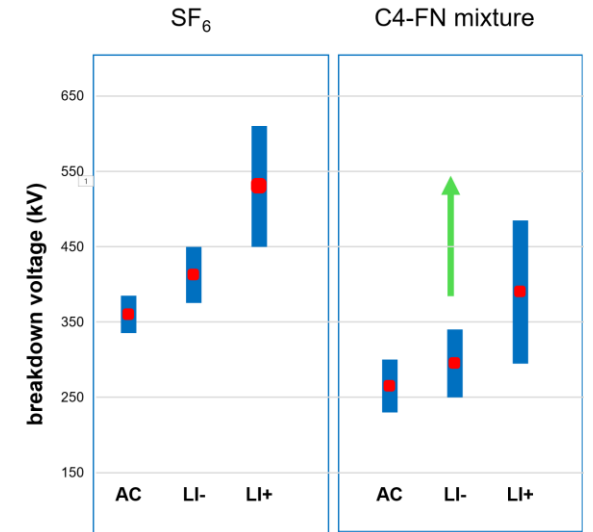
Different performance of C4-FN based mixtures vs. SF₆

- Lower critical electrical field
 - Lower breakdown voltage
 - > higher pressure and/or larger size required
 - “new” size close to 1990-2000 size

- CO₂ smaller molecule compared to SF₆
 - EPDM (Ethylene Propylene Diene Monomer) has high leakage
 - > butyl rubber

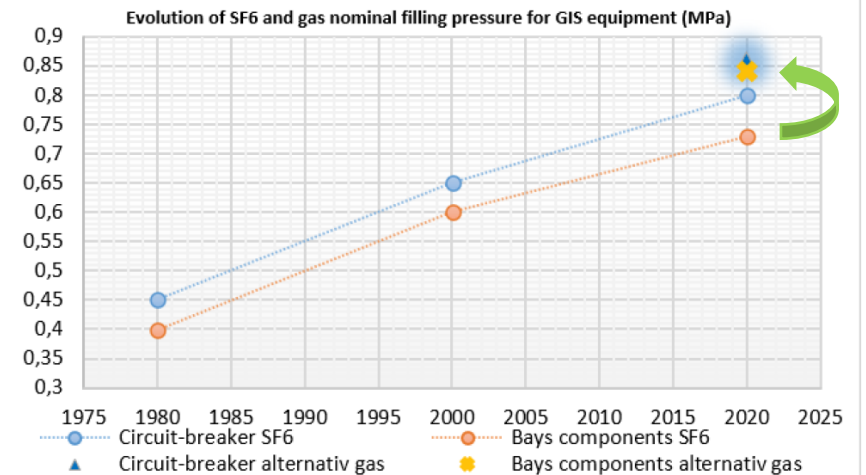
- Different thermal effusivity
 - Lower convective heat transfer (GIS)
 - > higher temperature rise

- High boiling point of fluorinated compounds
 - Limits “very cold” applications
 - > reduce the fraction of F-gas or leave out



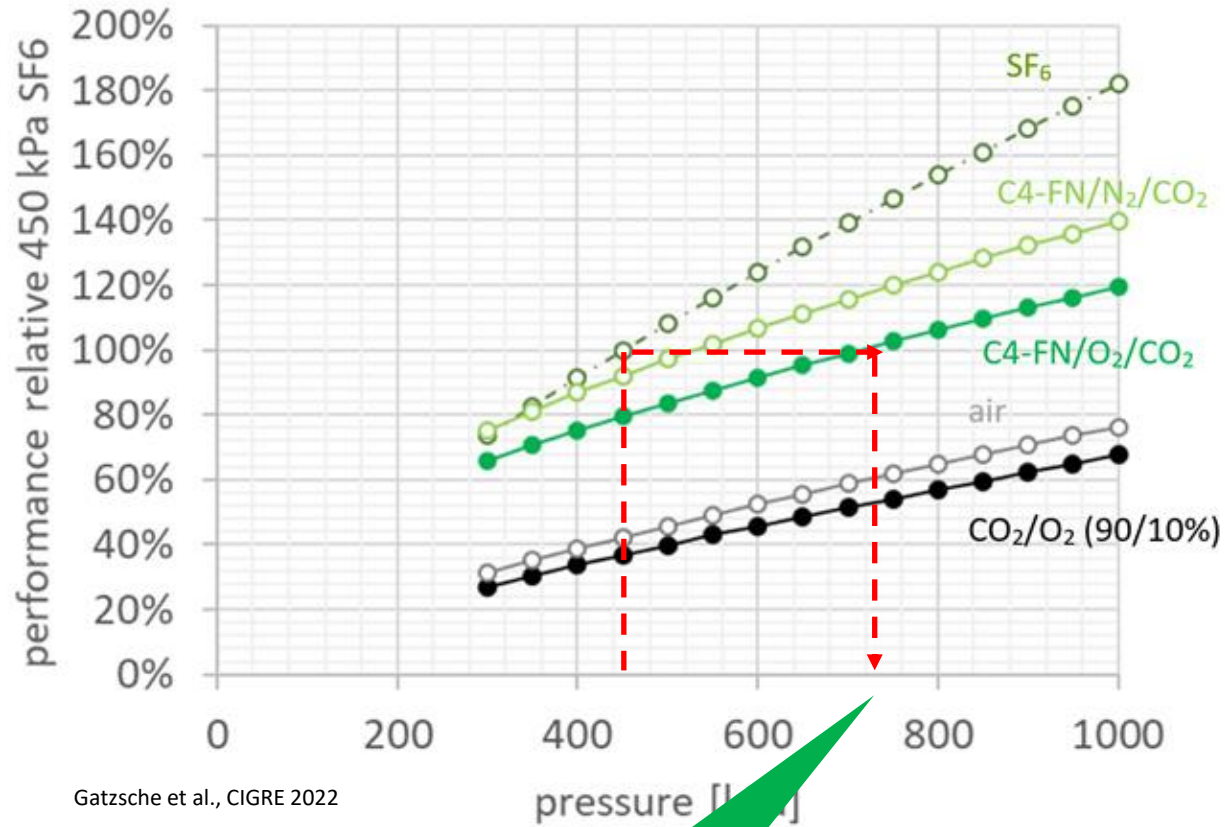
Pressure increase to force same footprint as SF₆

CIGRE TB 849, 2021



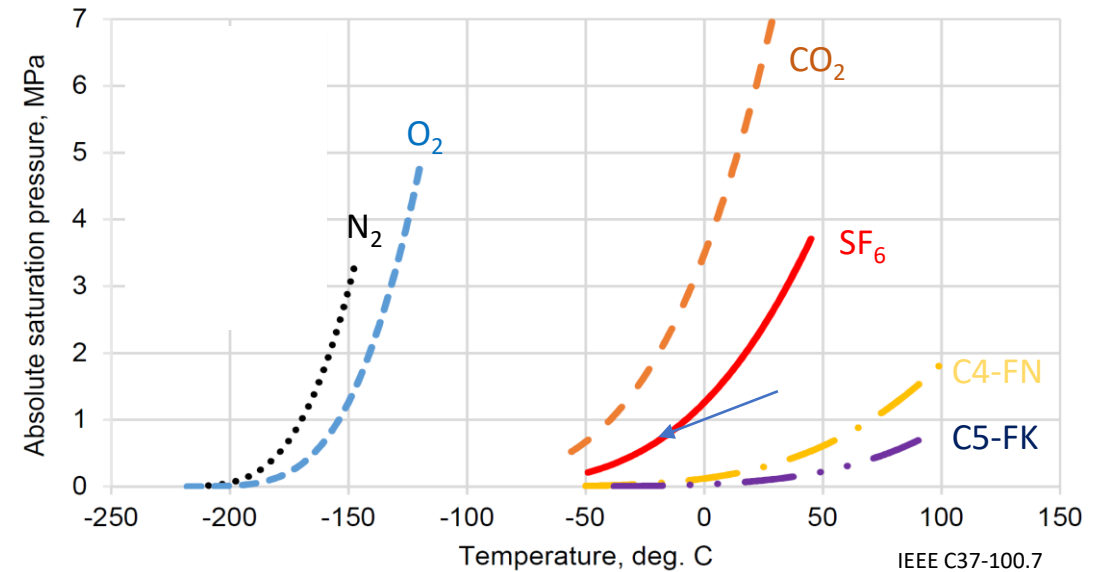
Blanchet, CIGRE Cairns 2023

Challenge: low minimum operation temperature



Gatzsche et al., CIGRE 2022

phase diagram
liquid <-> gas



- Higher gas pressure:
 - condensation at higher temperature
 - minimize the partial pressure of effective gas
- Not an issue with natural origin gases

Pressure increase 4.5 -> 7.5 b

Fault current interruption function: circuit breakers



live tank circuit breaker (LT)



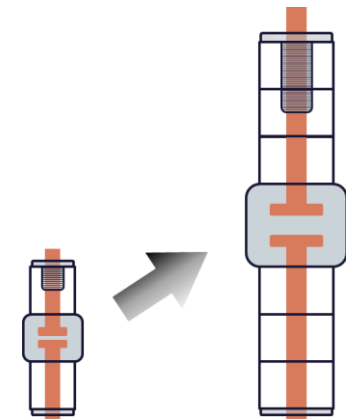
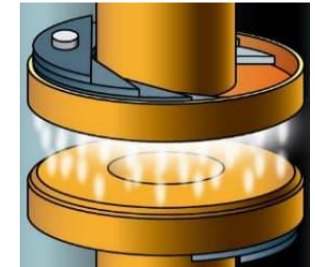
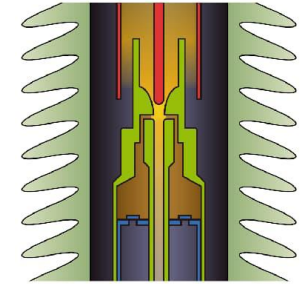
dead tank circuit breaker (DT)



GIS circuit breaker

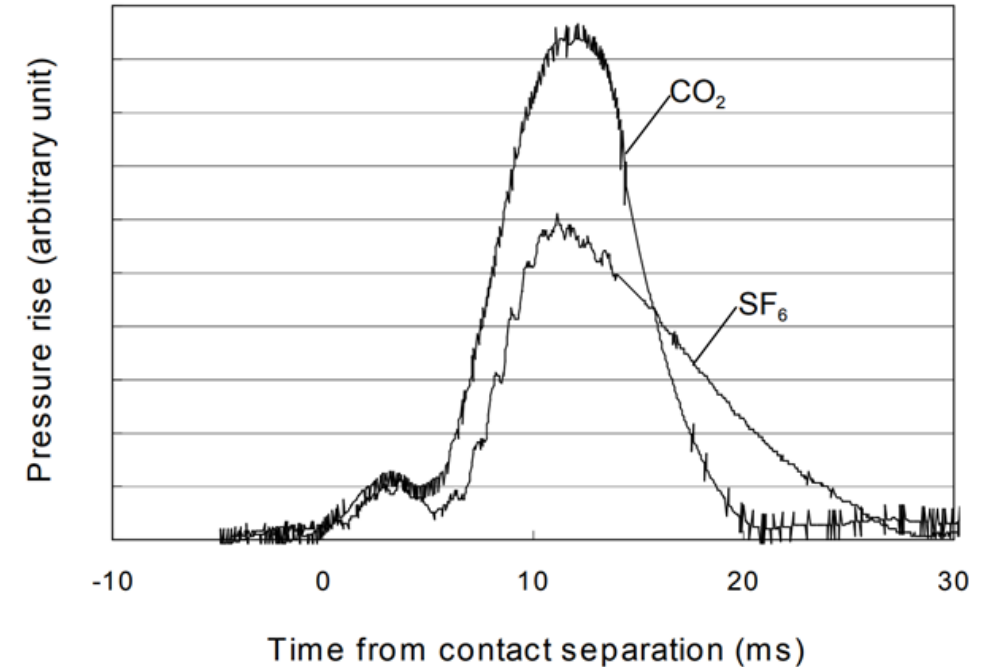
Two technologies:

- Gas (SF_6) circuit breakers
 - All voltage levels 10 – 1200 kV
 - outside insulation open air or SF_6
 - now available with SF_6 -free synthetic gases
- Vacuum circuit breakers
 - main workhorse in distribution
 - introduced in transmission (Japan > 2005)
 - originally with SF_6 outside insulation
 - now available with SF_6 -free insulation



Different performance of C4-FN mixture vs. SF₆ in interruption

- CO₂ has higher speed of sound
 - Faster flushing of the arcing zone
 - > Larger compression volume, valves re-design
- CO₂ has lower adiabatic index
 - High transient pressure during interruption
 - > re-enforce arcing chamber
- Lower critical electrical field
 - Affects recovery after interruption
 - > may require higher opening velocity
- Decomposition of fluorinated compounds under arcing
 - May impact electrical life
 - > have enough gas on board



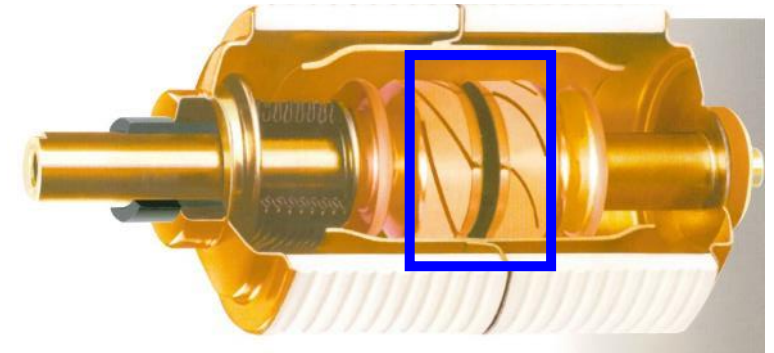
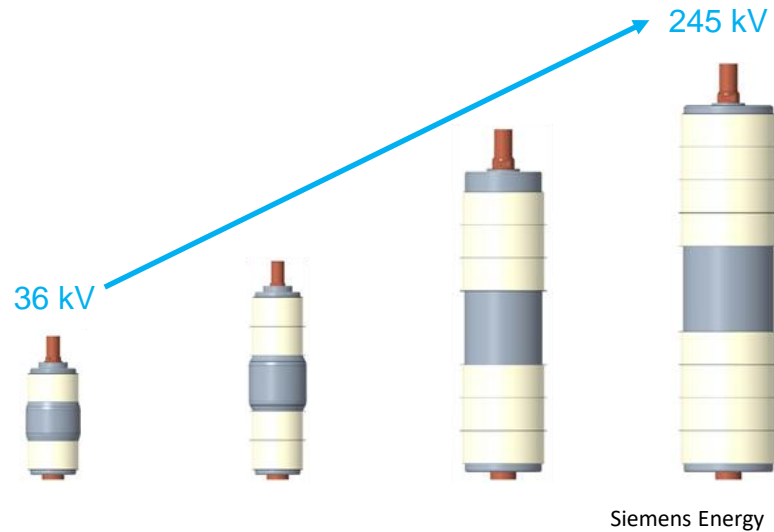
←→
arcing time

Uchii, T., et al. 'Fundamental research on SF₆-free gas insulated switchgear adopting CO₂ gas and its mixtures', In: Proceedings of the International Symposium on Eco Topia Science (2007).

Vacuum + compressed air for outside insulation

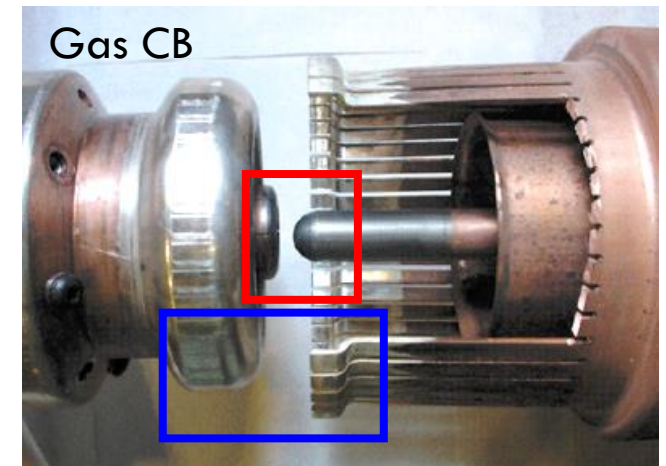
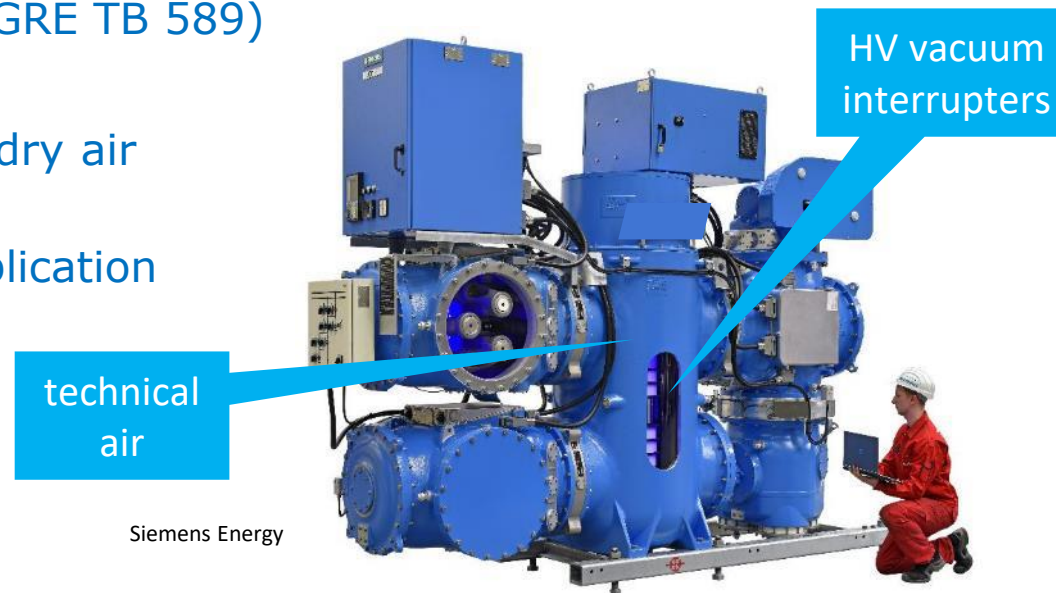
- Switching in vacuum
 - Well-proven in medium voltage
 - Very simple contact system

- A single contact system must:
 - Conduct current
 - Interrupt current (incl. fault)
 - Insulate



One contact set does it all

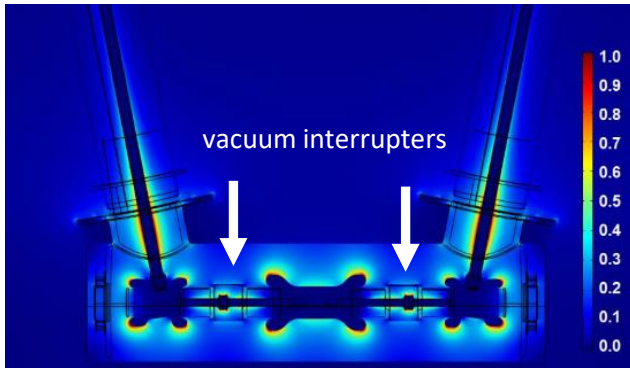
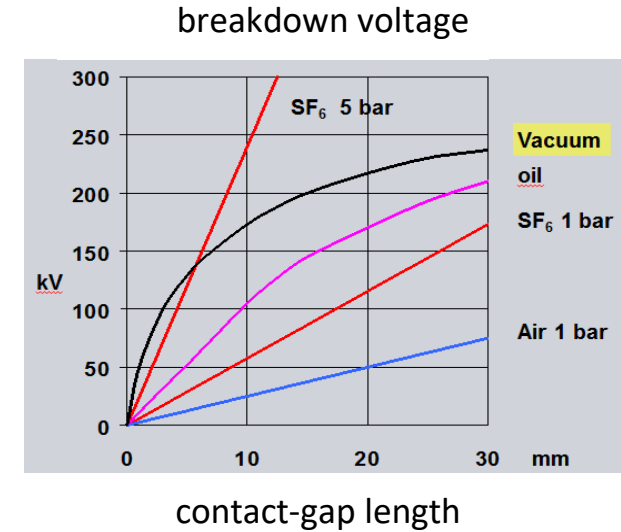
- Traditional designs for HV vacuum breakers have SF₆ as insulation
 - Over 10 000 in Japan (CIGRE TB 589)
- New designs use technical/dry air
 - Need higher pressure
 - Very low temperature application



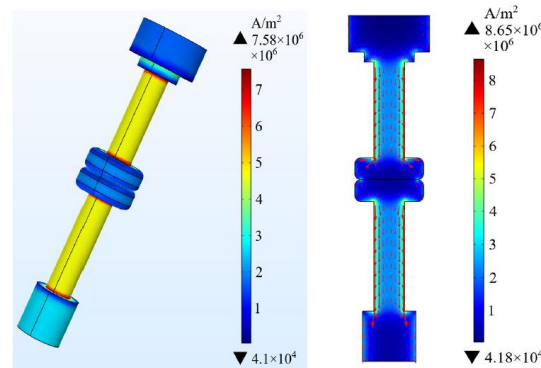
main contacts + arcing contacts

Differences of SF₆-free HV vacuum vs. MV vacuum: steady state

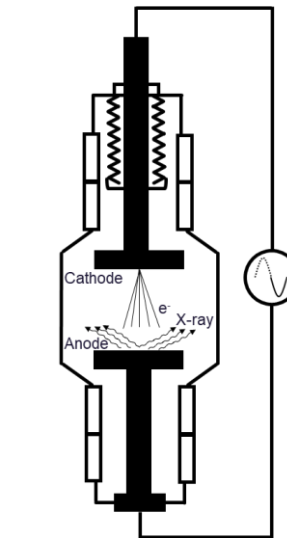
- Natural origin gases as outside insulator has lower critical electrical field
 - Lower breakdown voltage -> higher pressure and/or larger size
- Breakdown voltage not proportional to gap length
 - Increase of gap length no longer effective -> more interrupters in series
- One contact must perform all functions
 - Continuous current for transmission higher -> thermal management
- X-ray emission in open state -> shielding when testing



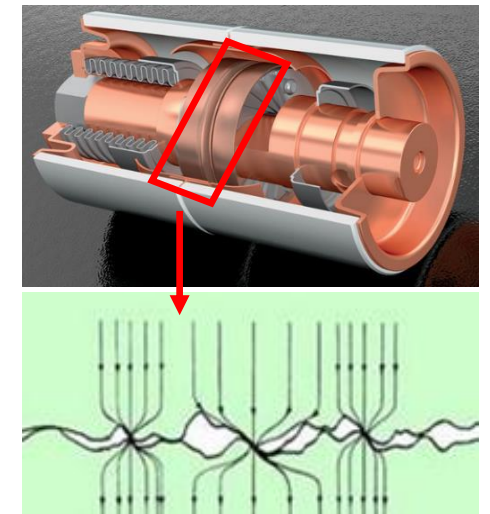
G. Nikolic et al., "Basic aspects of switching with series-connected vacuum interrupter units in high-voltage metal-enclosed and live tank arrangements", CIGRE Conference paper A3-112, 2020



X. Yu et al., "Investigation on the Thermal Performance of a 363 kV Vacuum Circuit Breaker Using a 3D Coupled Model", IEEE Access 2019, D011109/ACCESS.2019.2938313

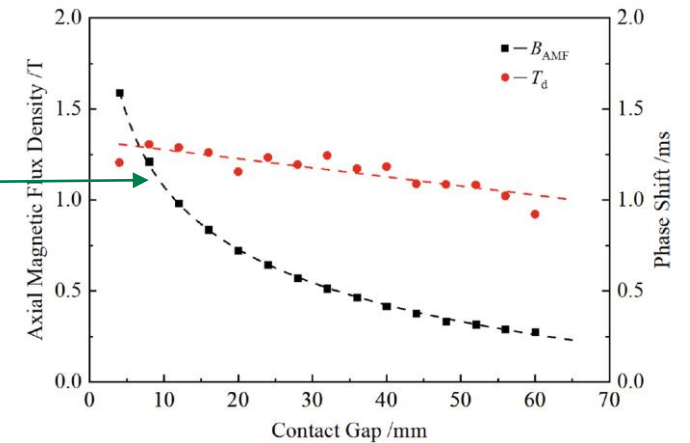
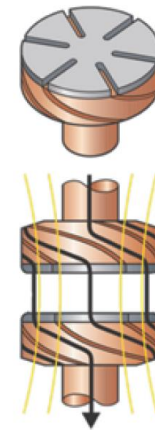


T. Heinz et al., "Why vacuum technology is not a simple scaling from medium to high voltage", ISDEIV 2023

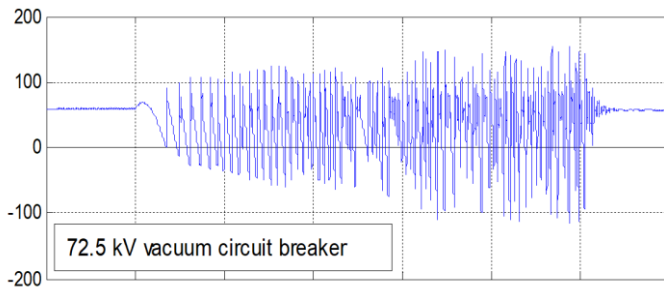


Differences of vacuum vs. SF₆ in current interruption

- Arc control with axial magnetic field becomes challenging
 - Special contact system design
 - May require multi-stage contact separation strategy
- Post-arc current much larger than in gas-breakers
 - Challenging for voltage grading in series connection
- Transients with inductive/capacitive switching
 - Multiple re-ignitions, restrikes -> mitigation



Z. Liu et al., "Switching Arc Phenomena in Transmission Voltage Level Vacuum Circuit Breakers", Springer, 2021



R. Smeets et al., "Switching in Electrical T&D Systems", Wiley, 2014

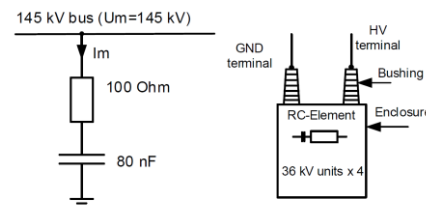
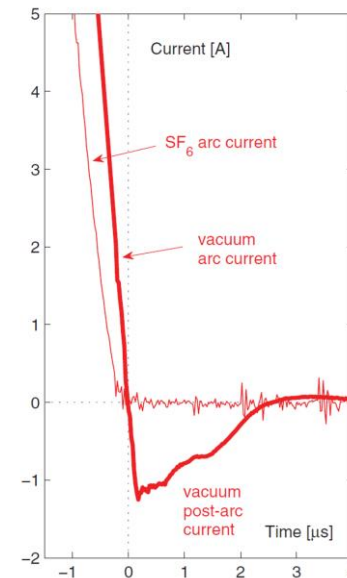
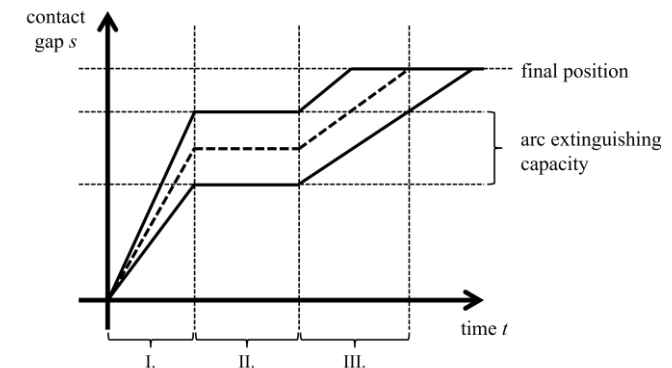


Fig. 7. Rating of RC suppressor for 145 kV system

K. Trunk et al., "Small Inductive Current Switching with High-Voltage Vacuum Circuit Breakers", ISDEIV conference 2021


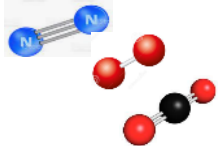
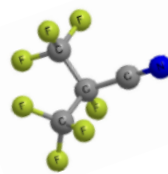


R. Smeets et al., "Switching in Electrical T&D Systems", Wiley, 2014
















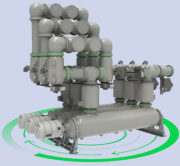









T. Heinz et al., "Control of Vacuum Arcs in High-Voltage Vacuum Interrupters by Suitable Stroke Trajectories of Opening AMF Contacts", ISDEIV 2018

SF₆ – free high-voltage equipment

	INSULATION	INTERRUPTION	GWP	VOLTAGE	APPLICATION
 SF ₆	SF ₆	SF ₆	25 200	24 – 1 200 kV	dist / LT / DT / GIS
natural-origin gases  N ₂ O ₂ CO ₂	AIR, N ₂ , solid	VACUUM	0	10 - 170 kV	dist / LT / DT / GIS
	O ₂ / CO ₂		1	72.5 - 145 kV	live tank
	TECHNICAL AIR		0	420 kV	GIB / GIL
fluoronitriles Novec™ 4710 C4-FN 	C4-FN / AIR	VACUUM C4-FN / AIR	300 - 750	10 - 40.5 kV	Distr / LBS / GIS
	C4-FN / O ₂ / CO ₂ mixture A		300 - 750	72.5 - 170 kV 420 kV in pilot	GIS live tank dead tank
	C4-FN / O ₂ / CO ₂ mixture B		300 - 750	170 kV	GIS
	C4-FN / CO ₂		> 500	1 000 kV	GIB GIL
	C4-FN / N ₂		300 - 750	420 kV	

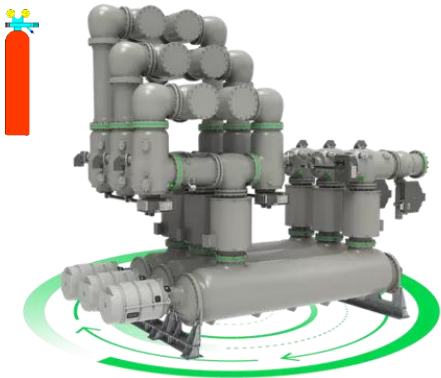


SF₆-free transmission switchgear 72.5 – 420 kV (examples)

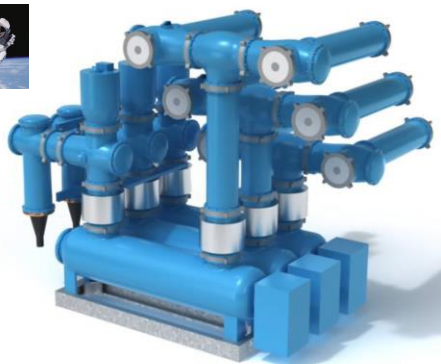
					 							
												
Design	GIS	GIS / LT	GIS	Live tank	GIS	GIS	GIS / LT	Dead tank	GIS	Recloser	Dead tank	GIS
Insulation	C4-FN mix	C4-FN mix	C4-FN mix	Dry air	C4-FN mix O ₂ -free	Dry air	Techn. air	Techn. air	C4-FN/ CO ₂	Solid	Dry air	Dry Air
Switching medium	C4-FN mix	C4-FN mix	C4-FN mix	O ₂ / CO ₂	C4-FN mix O ₂ -free	Vacuum	Vacuum	Vacuum	Vacuum	Vacuum	Vacuum	Vacuum
Volt. (kV)	170	145 -> 420	170 -> 420	145	170	170	145	72/84	170	72.5	145	72/84
Current (A)	3150	3150	1250	3150		4000	3150	1200	4000	2000	3150	
SC curr (kA)	50	40	50	40	50	50	40	31.5	50	31.5	40	
Fill. Press. (MPa)abs	0.8	0.85	0.83	1.2	0.85		0.8		0.75	0.8	1.0	-

Outlook into SF₆-free switchgear future

- Insulation
 - Gas insulated line / bus already in operation 420 -> 1000 kV
 - Switchgear development lagging (dual gas?)
- Interruption
 - up to 170 kV to approach SF₆
 - (when) can alternatives fully match SF₆?
 - Limit of single break vacuum?
- Multi-break technology
 - Pilots up to 420 kV starting

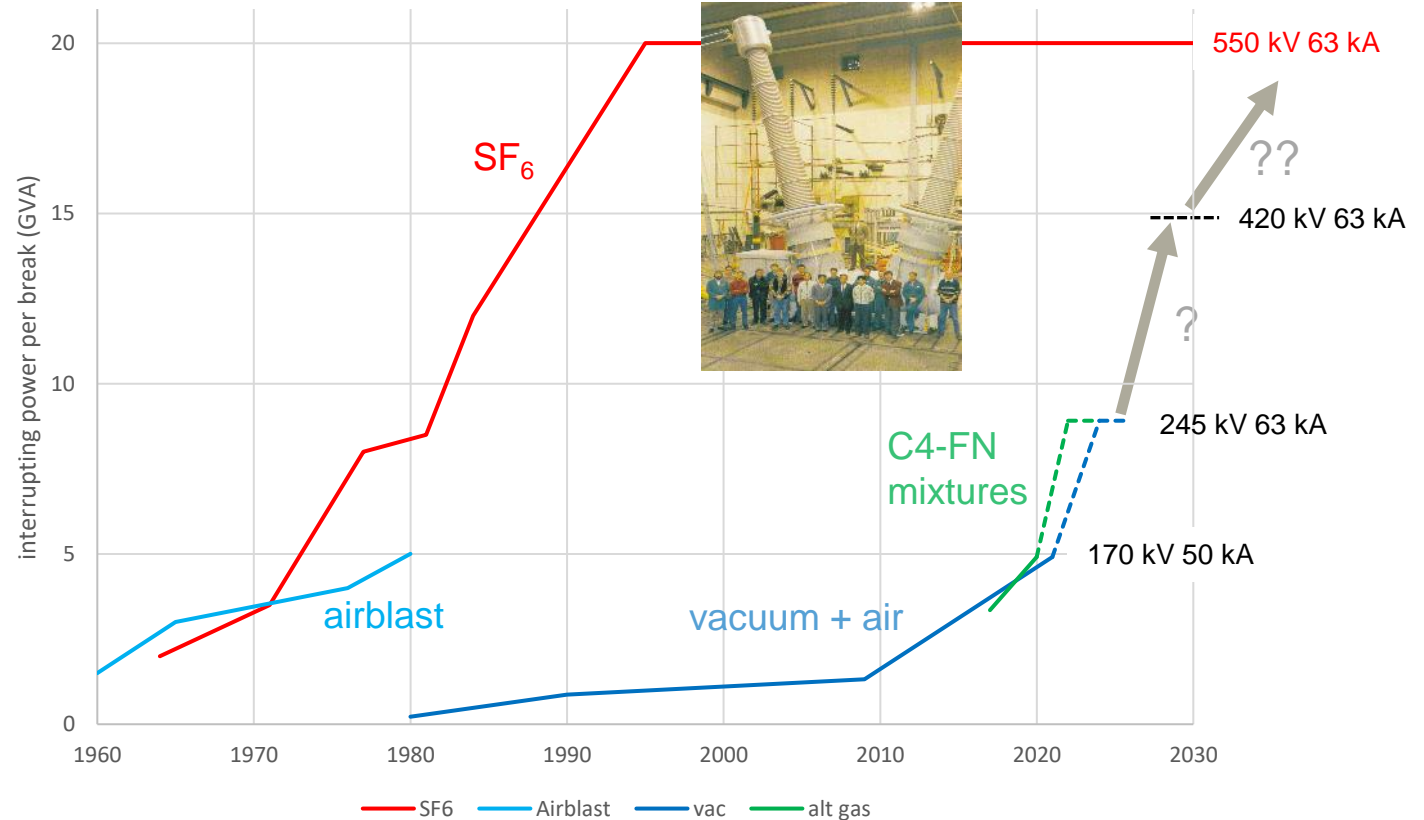


420 kV C4-FN mixture double break GIS
Hitachi Energy 2024



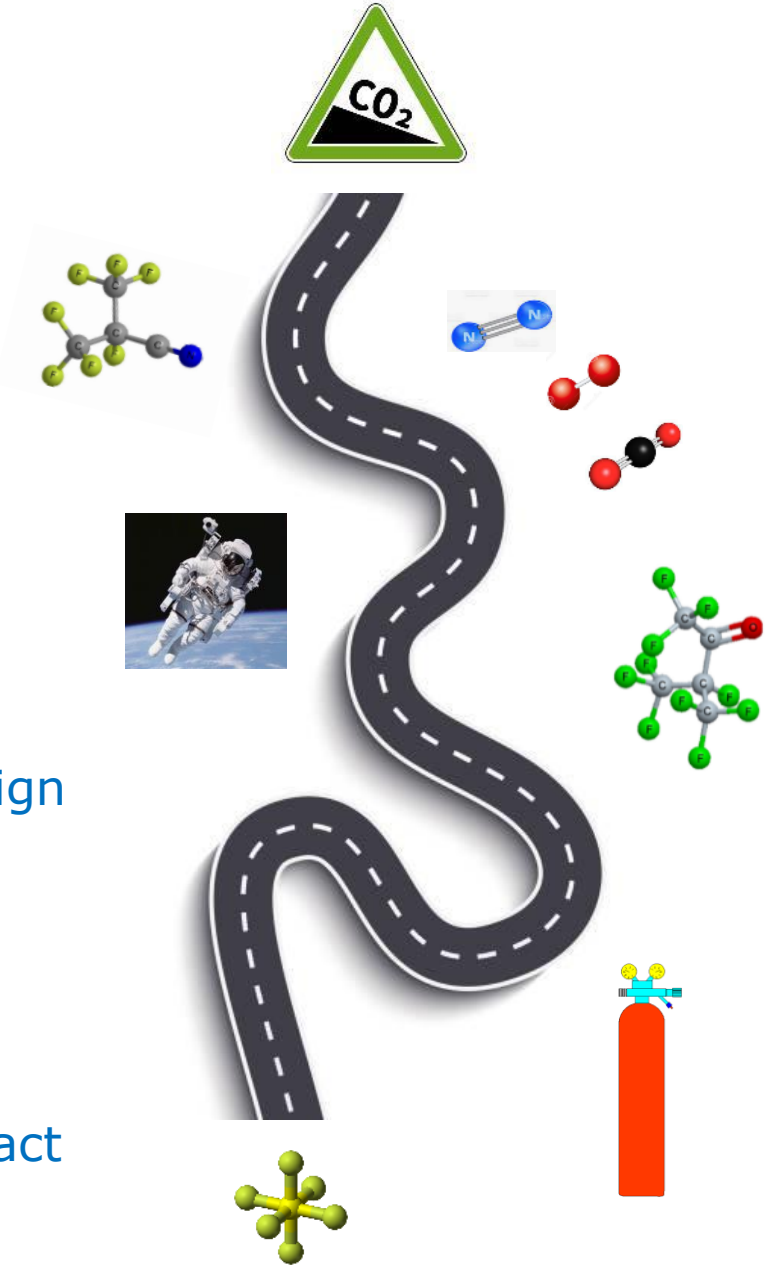
420 kV air insulated+double break vacuum
circuit breaker GIS. Siemens Energy > 2025

Interrupting power per break (GVA)



Status: Where are we now?

- SF₆-free GIS available up to 170 kV, 420 kV announced / in pilot
- SF₆-free GIL / GIB in pilot up to 1000 kV
- Three technologies for utility application:
 - Mixture of C4-FN with CO₂ / O₂ GWP 300 -750 HV -> EHV
 - Vacuum circuit breaker GWP < 1 MV -> HV
 - Mixture of CO₂ / O₂ GWP = 1 HV
- All new media are inferior to SF₆ but this can be overcome by design
 - Higher filling pressure
 - Redesign of key components
 - Acceptance of larger size, weight, cost
- New EU F-gas prohibitions plus upcoming restrictions on the production of PFAS (per- and polyfluoroalkyl) substances will impact applications in certain markets



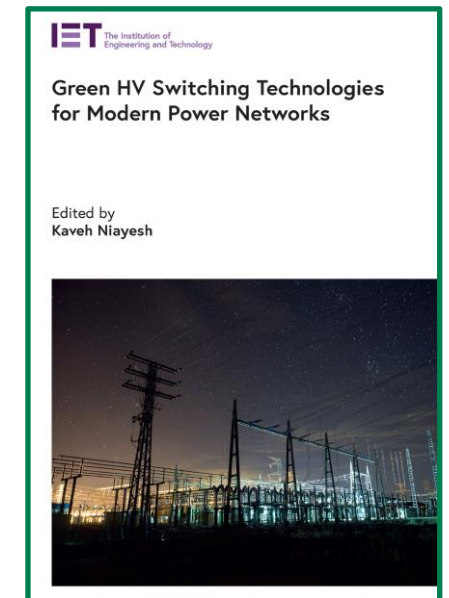
Independent industry activities



- **IEEE PES TR64** “Impact of Alternate Gases on Existing IEEE Standards” 2018 (Uzelac)
- **CIGRE WG B3.45** “Application of non-SF₆ gases or gas mixtures in medium voltage and high voltage gas-insulated switchgear. TB 802, 2020 (Knol)
- **T&D Europe** “Technical report on alternative to SF₆ gas in medium voltage & high voltage electrical equipment”, 2020
- **CIGRE WG D1.67** “Dielectric performance of new non-SF₆ gases and gas mixtures for gas-insulated systems”. TB 849, 2021 (Franck)
- **IEC 62271-4 ED-2** “Handling procedures for gases and gas mixtures for interruption and insulation”, 2022
- **CIGRE WG A3.41** “Interruption and switching performance with SF₆ free switching equipment”. TB 871, 2022 (Smeets)
- **IEEE C37.100.7** “Draft guide for the Evaluation of Performance Characteristics of Non-Sulfur Hexafluoride Insulation and Arc Quenching Media for Switchgear Rated above 1000 V”, 2023 (Schiffbauer)
- **CIGRE WG B3/A3.60** “User guide for non-SF₆ gases and gas mixtures in substations“ -> 2024 (Knol)



2022, on SF₆ –free switching



2023, on SF₆ alternatives and DC

Thank you for your kind attention!

Next event: CIGRE Paris Conference Monday Aug 26, afternoon:
Workshop “Driving T&D substations and equipment towards zero emissions”

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1 February 2024

Towards net-zero emission of T&D grids

